

Adsorption of Aqueous Glyphosate N-Phosphonomethylglycine by Manganese Oxides/Mesoporous Silica SBA-15 Composite at High Salinity Condition

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Glyphosate N-phosphonomethylglycine (PMG) is the broad-spectrum herbicide used commonly around the world and the main feature of its production wastewater is high salinity. In this paper, the glyphosate removal by manganese-oxides-coated mesoporous silica SBA-15 (MnO₂/SBA-15) under high background salinity conditions was examined. A chemical precipitation method was employed for MnO₂ coating on an ordered mesoporous silica SBA-15 template to obtain a significantly enlarged BET surface area of the adsorbent, which was 963 m²/g. The maximum glyphosate uptake capacity for MnO₂/SBA-15 was found to be about 300 mg/g. The Langmuir equilibrium model was found to be suitable for describing the adsorption. Kinetic study showed that the adsorption fitted a pseudo-second-order kinetic model. The effects of different parameters such as pH and coexisted ions were also studied. The results also indicate the potential of adsorbents prepared by coating manganese oxides on porous materials *via* chemical precipitation in removing glyphosate from high-salinity wastewater.

Key Words: Manganese oxides, MnO₂/SBA-15, Glyphosate N-phosphonomethylglycine, High salinity, Adsorption.

INTRODUCTION

Glyphosate N-phosphonomethylglycine (PMG) is a highly effective broad-spectrum, post-emergence and non-selective herbicide that is widely used in agriculture worldwide^{1,2}. Many manufactures and reports claim that the use of glyphosate N-phosphonomethylglycine is safe for the environment³, but recent studies have showed that PMG may alter several vital biochemical processes in plants and microorganisms^{4,5}, increase the mobility and bioavailability of some soilmetal and correspondingly increase its environmental risk⁶. The United States Environmental Protection Agency (USEPA) has set maximum contaminant level (MCL) of 700 µg/L for drinking water.

Glyphosate N-phosphonomethylglycine production industries generate large quantities of high salinity wastewater. Various treatment processes have been investigated to reduce glyphosate concentrations in water and to minimize the potential health risks, including electrooxidation⁷, biotreatment^{8,9}, electric field-assisted biosorption¹⁰, nanofiltration¹¹ and photodegradation¹². Among the problems encountered in the use of these techniques are high investment and operation cost. Adsorption is an ideal and appropriate technique because of its simplicity and cost effectiveness. PMG has three groups (amino, carboxylato and phosphonato) that enabled it to coordinate strongly to mineral surfaces¹³⁻¹⁵. It is commonly believed that the formation of surface complexes through the phosphonate group is predominant, while the amine and carboxylate groups remain relatively free from complexation^{16,17}. Adsorption of PMG on natural materials such as goethite^{16,18,19}, manganite^{20,21} and aluminum hydroxides²² has been reported. However, high salt content in wastewater is known to significantly reduce the treatment efficiency of these natural adsorbents. Several materials have been synthesized and investigated for their glyphosate adsorption capacity such as MgAl-layered double hydroxides²³ and Ni₂AlNO₃ layered double hydroxide²⁴, with adsorption capacity around 30 and 200 mg/g, respectively. However, there is still scope for improving the sorption capacity and simplifying the adsorbent preparation.

Many low cost porous materials, such as activated carbon, amorphous silica and some clay minerals, would be used as the template to enlarge the surface area of the adsorbent. These low cost porous materials, however, have both microporous and mesoporous structure, which would disturb the investigation of the adsorption of glyphosate by the adsorbent. Mesoporous material contains pores with diameters between 2 and 50 nm, which allows a smooth diffusion of molecules in the pores²⁵. Shin *et al.*²⁶ have found that, compared with activated alumina, Al-impregnated mesoporous materials show fast adsorption kinetics as well as high adsorption capacities. It was also reported that, the pores SBA-15 can be adjusted from 2-10 nm in a narrow diameter distribution region simply by changing the experimental conditions²⁷. Therefore mesoporous silica SBA-15 was chosen as the template in order to clearly investigate the alterations after coating of MnO_2 into the channels and the adsorption performance of PMG on ordered mesoporous materials.

This study, therefore, synthesized a novel $MnO_2/SBA-15$ composite adsorbent for effective PMG removal from waters with greatly enhanced surface area achieved by a chemical precipitation process of MnO_2 on an ordered SBA-15 template. The adsorption of PMG by the $MnO_2/SBA-15$ composite from aqueous solutions was investigated as a function of the contact time, initial PMG concentration, ionic strength, pH value and coexisted anions of the aqueous solution.

EXPERIMENTAL

Surfactant pluronic P123, *i.e.*, triblock poly(ethylene oxide)-poly(propylene oxide)-poly(ethylene oxide) (PEO₂₀PPO₇₀PEO₂₀), was employed as the structure-directing agent for SBA-15 and tetraethoxysilane TEOS; (CH₃-CH₂O)₄Si. have been employed as silica precursors. PMG from Fluka was used in adsorption experiments. All reagents were of analytical grade purchased from Aldrich.

Sample preparation: Preparation of SBA-15 was performed at State Key Laboratory of Pollution Control and Resources Reuse, Nanjing University, using the method reported by Kim *et al.*²⁸.

The manganese dioxide coated mesoporous silica SBA-15 (MnO₂/SBA-15) was prepared by a chemical precipitation process. 5 g SBA-15 was immersed in 50 mL of MnCl₂ solution at various concentrations and the pH was adjusted to 3.3. The suspension was vigorously stirred at room temperature with no pH control. Meanwhile 1.7 g of KMnO₄ was added to the suspension, immediately making the solution dark brown, which indicated the formation and precipitation of MnO₂:

 $3Mn^{2+} + 2MnO_4^{-} + 2H_2O = 5MnO_2\downarrow + 4H^+$

Finally, the suspension was filtered, washed with highpure water and dried at 105 °C for 4 h.

The $MnO_2/SBA-15$ composite was characterized by transmission electron microscopy (TEM) to evaluate the alterations of the surface and channels, whereas the surface area was calculated using the Brunauer-Emmett-Teller method.

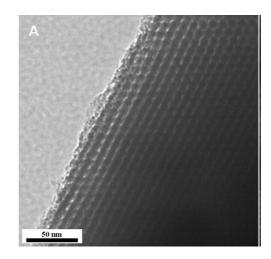
Batch adsorption experiments: Batch adsorption experiments were conducted to examine the effects of adsorbent dose, contact time, initial PMG concentration, ionic strength, solution pH, as well as coexisted anions on adsorption performance. Single runs were carried out by stirring 200 mg of $MnO_2/SBA-15$ composite in 25 mL of aqueous PMG solutions at 150 rpm and 25 °C. A preliminary kinetic test revealed that adsorption equilibrium of PMG on $MnO_2/SBA-15$ composite was completely achieved within 24 h under the experimental conditions. Therefore, an equilibrium time of 24 h was adopted for all the adsorption tests. Mixtures were filtered with a syringe filter of 0.22 µm and the final solutions were collected. The PMG concentrations in both the initial and final solutions were evaluated UV-VIS spectroscopy and the absorbance was measured

around 243 nm^{23} . The typical experimental error was kept lower than 5 % for all the experimental results.

RESULTS AND DISCUSSION

Optimization and surface characterization: Coating MnO_2 on SBA-15 could not only increase the amount of active sites but also affect the micro-porous structure of SBA-15, which play an important role in the sorption process. Thus it is necessary to determine the optimal amount of MnO_2 that coated onto the SBA-15. The modified samples obtained at various concentrations (0.2, 0.3, 0.4, 0.6 mol/L) of $MnCl_2$ solution were investigated in batch adsorption experiment.

As shown in Fig. 1, the adsorption capacity of the MnO₂/SBA-15 composite increases with the increase of the quantity of the MnO₂ coated on SBA-15 from 0.2-0.4M MnCl₂ and decreased with the increase of the quantity of the MnO₂ coated on SBA-15 from 0.4-0.6M MnCl₂. The adsorption capacities of the coated SBA-15 obtained with a 0.4M MnCl₂ solution are higher than those achieved with other coated SBA-15 and at least ten times greater than those of uncoated SBA-15. Therefore, this MnO₂/SBA-15 composite specimen was chosen as the sample in the following characterization and batch adsorption experiment. The amount of manganese on the surface of the MnO₂/SBA-15 composite, measured through acid digestion analysis was approximately 62.4 mg Mn/g MnO₂/SBA-15 composite.



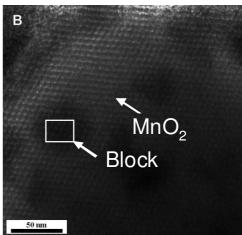


Fig. 1. TEM images of (A) uncoated SBA-15;(B) MnO₂/SBA-15 composite

Microstructure of SBA-15 and MnO₂/SBA-15 were investigated by TEM technique (Fig. 2A-B). TEM images evidenced that the well-ordered hexagonal structure of SBA-15 is maintained during the incorporation of MnO₂ chains into the channels. The black dots marked by the arrows were the MnO₂ forming within the channels of SBA-15 and the dark areas marked by the rectangle were the channels blocked by MnO₂. The BET surface areas were 1012 and 963 m²/g for SBA-15 and MnO₂/SBA-15, respectively, indicating the heap of MnO₂ within some channels.

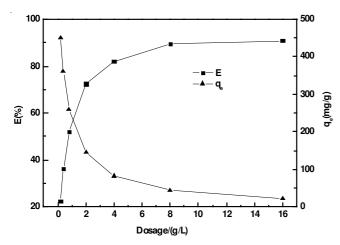


Fig. 2. Adsorption of PMG on MnO₂/SBA-15 composite as a function of adsorbent dosage. PMG initial concentration = 400 mg/L; ionic strength = 1M NaCl; T = 298 K; pH = 4.0

Amount of adsorbent: Fig. 3 shows the effect of adsorbent dose on the removal of PMG at pH 4 and initial PMG concentration of 400 mg/L for 24 h. At 0.2 g/L of the adsorbent dose, 14.7 % of PMG was removed and gradually increases up to 84.1 % at 8 g/L of adsorbent and then continued to increase at lower speeds from 84.1-86.2 % at 16 g/L of adsorbent. Therefore, 8 g/L MnO₂/SBA-15 is used in the following tests as the optimum adsorbent amount. The increase of the sorbent dosage leads to the decrease in q_e as there are too many adsorbent for the limited amount of PMG. And the PMG removal percentage increases with the dosage until equilibrium²⁹. The saturation adsorbent capacity is fixed.

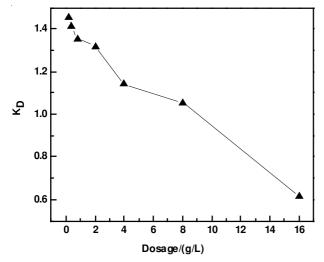


Fig. 3. Plot of K_D value as a function of adsorbent dosage

A distribution coefficient K_D , which reflects the binding ability between the adsorbent surface and PMG, was showed in Fig. 4. K_D is dependent on pH of the solution and type of surface of the adsorbent³⁰. The distribution coefficient values of PMG adsorbed on MnO₂/SBA-15 composite was computed using the following equation³¹:

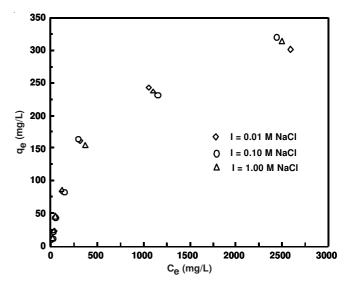


Fig. 4. Sorption isotherms of PMG by MnO₂/SBA-15 composite at three levels of ionic strength (0.01, 0.10 and 1.00 M NaCl), pH = 4.0, adsorbent dosage = 8 g/L, PMG initial concentration at 100, 200, 400, 800, 1600, 3000, 5000 mg/L

$$K_{\rm D} = \frac{C_{\rm s}}{C_{\rm w}} \,({\rm m}^3/{\rm kg}) \tag{1}$$

where C_s is the concentration of PMG on the solid particles (mg/kg) and C_w is the equilibrium concentration in water solution (mg/m³). If the surface of the adsorbent is homogeneous, the K_D values would not change with the adsorbent dosage³¹. As illustrated in Fig. 4, the K_D value decreased with an increase in adsorbent dose. It implies that the surface of the MnO₂/SBA-15 composite is heterogeneous.

Sorption isotherms and influence of ionic strength: Generally, for conventional adsorbents such as activatedcarbon, glyphosate adsorbs very strongly in distilled water but has a much lower capacity in high salinity water. Fig. 5 shows the adsorption isotherms of PMG onto MnO₂/SBA-15 composite covering a wide range of ionic strengths (0.01, 0.10 and 1.00 M) and PMG concentrations. As illustrated in Fig. 5, the maximum uptake capacities for PMG at 0.01, 0.10 and 1.00 M ionic strengths are about 298, 312 and 285 mg/g, respectively. The adsorption of PMG occurs over a wide range of ionic strength and the maximum adsorption took place at 1 M. Also, adsorption was always higher at any ionic strength for MnO₂/SBA-15 when compared to plain SBA-15. This will have an implication in the treatment of PMG production wastewater where the ionic strength is around 1 M. In depth studies have been done to establish the mechanism of adsorption of PMG onto coated SBA-15 which is discussed in the following sections.

Both the Langmuir eqn. 2 and the Freundlich equations eqn. 3 were used to describe the adsorption isotherms.

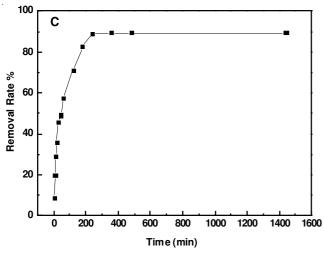


Fig. 5. Dynamics for PMG removal by MnO₂/SBA-15 composite. PMG initial concentration = 400 mg/L; ionic strength = 1M NaCl; adsorbent dosage = 8 g/L; T = 298 K; pH = 4.0

Langmuir:
$$Q_e = \frac{K_L Q_m C_e}{1 + K_L C_e}$$
 (2)

 $Q_e = K_F C_e^{\frac{1}{n}}$ where C_e (mg/L) is the equilibrium concentration of PMG, q_e

(3)

(mg/g) the amount adsorbed under equilibrium, $q_m (mg/g)$ the theoretical maximum adsorption capacity of the adsorbent for PMG, K_L (L/mg) a Langmuir binding constant related to the energy of adsorption, K_F and n the Freundlich empirical constants.

Table-1 shows the Langmuir and Freundlich isotherm constants. It can be seen that the Langmuir shows significantly higher correlations ($R^2 \ge 0.99$) than the Freundlich model. Because the Langmuir model is based on the physical hypothesis that the maximum adsorption capacity consists of a monolayer adsorption, it is evident that the adsorption of PMG by MnO₂/SBA-15 composite is a monolayer adsorption. The theoretical maximum adsorption capacities (q_m) at the three ionic strengths (0.01, 0.10 and 1.00 M) are about 297.6, 299.6 and 307.4 mg/g, respectively, which are in good accordance with experimental data.

TABLE-1 LANGMUIR AND FREUNDLICH PARAMETERS OF PMG ADSORPTION ISOTHERMS BY MnO₂/SBA15 COMPOSITE Langmuir model Freundlich model I Q KL (mol/L) \mathbb{R}^2 \mathbb{R}^2 K n (mg/g)(L/g)0.01 297.6 0.0036 0.9997 3.60 1.66 0.9637 0.10 299.6 0.0035 0.999 3.45 1.63 0.9596 1.00 307.4 0.0032 0.9993 3.34 1.62 0.9543

Kinetic studies: Influence of contact times up on the adsorption of PMG were recorded at adsorbate concentration of 400 mg/L as shown in Fig. 6. Adsorption of PMG increased fast in the first 3 h and then decreased and attained equilibrium at 4 h, indicating that the adsorption sites in the pores of the SBA-15 are not well exposed. Kinetic data of PMG sorption onto MnO₂/SBA-15 were studied with pseudo-first and

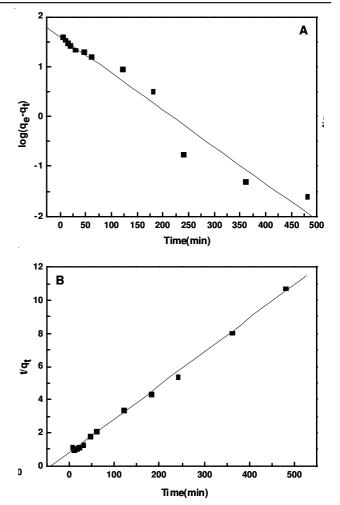


Fig. 6. (A) Pseudo-first-order kinetics of PMG sorption by MnO₂/SBA-15 composite. B: pseudo-second-order kinetics of PMG sorption by MnO₂/SBA-15 composite

pseudo-second order kinetic models. The mathematical representations of models are given in eqns. 4 and 5, respectively.

$$lg (q_e - q) = lg q_e - K_1 t$$
(4)

$$\frac{t}{q} = \left(\frac{1}{K_2 q_e^2}\right) + \left(\frac{t}{q_e}\right)$$
(5)

where K_1 (min⁻¹) represents the rate constant, q_e (mg/g) the amount of PMG adsorbed on the adsorbent surface at equilibrium, K₂ the pseudo-second-order rate constant (g mg⁻¹ min⁻¹) and q (mg/g) the amount of PMG adsorbed at any time t (min).

The adsorption rate constant (K_1) in 480 min for PMG adsorption was calculated from the slope of the linear plot of lg (q_e-q_t) versus time (Fig. 7A). K₂ could be determined from the slope and interception by plotting t/q versus t (Fig. 7B). The rate constants obtained from first- and second-order pseudo-kinetic models are given in Table-2. The entire kinetic data fitted well with pseudo-second-order reaction rate model, which is evident from the higher correlation coefficient values. Also, the adsorption capacities calculated by the model are close to those results obtained from experiments. These results suggest that chemical adsorption involving valency forces may limit the PMG adsorption process.

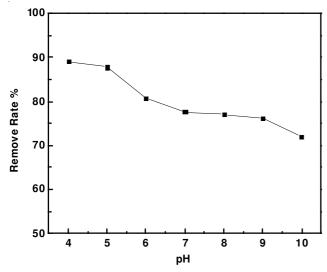


Fig. 7. Effect of solution pH on PMG removal by MnO₂/SBA-15 composite. PMG initial concentration = 400 mg/L; ionic strength = 1M NaCl; adsorbent dosage = 8 g/L; pH adjusted by HCl and NaOH solutions; the pH value is the pH of the solution at equilibrium

TABLE-2 PARAMETERS OF KINETIC MODELS OF PMG ADSORPTION ONTO MnO ₂ /SBA-15			
q _e exp (mg/g)	Pseudo-first-order model in 480 min		
	$K_{1}(min^{-1})$	q _e calcd. (mg/g)	\mathbb{R}^2
44.7	7.4×10^{-3}	38.34	0.9572
q _e exp (mg/g)	Pseudo-second-order model in 480 min		
	$K_2 (g mg^{-1} min^{?1})$	q _e calcd. (mg/g)	\mathbb{R}^2
44.7	5.07×10^{-4}	46.26	0.9977
44.7	$\frac{K_{1} (min^{-1})}{7.4 \times 10^{-3}}$ Pseudo-secon $K_{2} (g mg^{-1} min^{?1})$	q _e calcd. (mg/g) 38.34 nd-order model in 48 q _e calcd. (mg/g)	R ² 0.9572 0 min

Influence of pH: Generally, pH is an important factor affecting the adsorption process. Fig. 8 presents the PMG removal after adsorption at different initial pH values, ranging from 4-10. PMG adsorption was found to decrease with increasing pH values. When PMG get into the channels of MnO₂/SBA-15 composite, there are essentially three types of phosphonate bonds responsible for the adsorption mechanisms, *i.e.*, uncomplexed P-O (I), intramolecularly hydrogen bonded P-O (II) and surface complexed P-O (III)¹⁶. Therefore, the proposed stoichiometries and structures of PMG-MnO2 surface complexes could be described as Scheme-I, *i.e.*, single handed ligand between PMG and manganite (Scheme-I-A) and the bidentate binuclear bridging PMG-manganite complex (Scheme-I-B). The single handed ligand of PMG and manganite group would be easily affected by hydration while the bidentate binuclear bridging PMG-manganite group complex is independent of hydration process including pH conditions. Thus, the adsorption of PMG by MnO₂/SBA-15 can be modeled as a chemical adsorption as single handed ligand between PMG and manganite.

Effect of interfering anions: Usually in wastewater many ions such as nitrate, sulfate and phosphate are present and these compete with PMG during adsorption. Fig. 9 shows the effect of these anions on the adsorption of PMG onto MnO_2/SBA -15. The initial concentration of PMG was fixed (500 mg/L) whereas the concentration of sulfate, phosphate, chloride and nitrate was varied in the adsorption test. It can be seen that SO_4^{2-} and NO_3^{-} has not shown significant interference in PMG

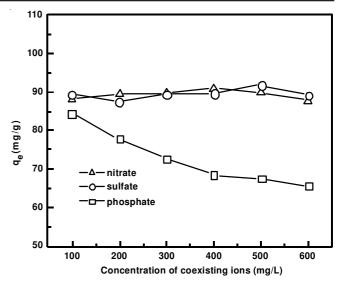
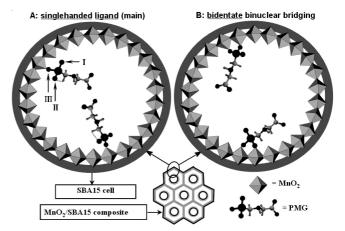


Fig. 8. Effect of coexisted anions (nitrate, sulfate and phosphate at the concentrations of 100, 200, 300, 400, 500 and 600 mg/L) on PMG removal by MnO₂/SBA-15 composite. PMG initial concentration = 500 mg/L; inoic strength = 1M NaCl; pH = 4.0; adsorbent dosage = 8 g/L



Scheme-I: Proposed stoichiometries and structures of PMG- MnO₂ surface complexes

uptake. By contrast, the adsorption of PMG decreased with increase in phosphate concentration. This could be attributed to their competence with PMG for the active sites. This result is also evident for the assumption that PMG adsorption process was controlled by chemical process.

Conclusion

In this study, manganese-oxide-coated mesoporous silica SBA-15 was prepared *via* chemical precipitation. The SBA-15 template supplied a large surface area of 963 m²/g for the coating of MnO₂, which provided plentiful binding sites for PMG adsorption. The MnO₂/SBA-15 composite is capable of maintaining a high PMG adsorption capacity under high salinity conditions (1M NaCl), with a maximum adsorption capacity of over 300 mg/g. The adsorption isotherms were well described by Langmuir model. It was found that the pseudo-second-order model better represented the sorption kinetics in the PMG adsorption, suggesting that the PMG adsorption process by MnO₂/SBA-15 composite is controlled by chemical process. The adsorption of PMG by MnO₂/SBA-

15 can be modeled as the formation of singlehanded ligand between PMG and manganite. The result indicates an important role of MnO₂/SBA-15 composite as a potential adsorbent for removal of organophosphate and organophosphonate pollutants from high salinity wastewater.

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