



## Viscosity and Antiwashout Properties of Cement Mortar at Low Temperature Seawater Environment†

HEON CHANG KIM<sup>1</sup>, IN-KYU JANG<sup>2</sup> and SEUNG-KYU PARK<sup>1,\*</sup>

<sup>1</sup>Department of Chemical Engineering, Hoseo University, Asan 336-795, Republic of Korea

<sup>2</sup>GENOSS Ltd., Suwon 443-270, Republic of Korea

\*Corresponding author: Fax: +82 41 5405758; Tel: +82 41 5409686; E-mail: [skpark@hoseo.edu](mailto:skpark@hoseo.edu)

Published online: 10 March 2014;

AJC-14839

Cement mortar is a construction material and generally a mixture of water, cement, sand and sometimes fine gravel. When cement mortar is applied to the seawater construction at low temperature below 0 °C, the flow performance, workability, placement, antiwashout and consolidation should be considered in combination. In this research, the antiwashout and rheological properties of the cement mortar have been investigated with admixtures prepared by adding anionic surfactants, cationic surfactants and polymeric thickeners. Cement mortar formulated by pseudo-polymeric systems, electrostatic association of anionic and cationic surfactants and polymer additive such as poly methyl vinyl ether, showed thixotropic, suitable antiwashout, proper workability and self-leveling properties. Addition of isopropyl alcohol to mixed surfactant admixture decreases the freezing temperature of cement grout to -7 °C and increases the workability at cold seawater, but slightly decreases the compressive strength of the cement grout at seawater system.

**Keywords:** Cement mortar, Antiwashout, Thixotropic, Mixed surfactant, Cold seawater.

### INTRODUCTION

In recent years, numerous studies have been done on the interfacial properties of mixtures of various surfactants. For the description of the properties of surfactant blends, the mutual interactions of surfactants as well as their interactions with adjacent phases have been considered. For mixed micelle formation, a simple physical interaction as non-ideal mixtures is possible<sup>1</sup>. When anionic and cationic surfactants are dissolved in water, the surfactants can be present in three different environments: as monomers, incorporated in mixed micelles and as precipitate<sup>1,2</sup>. It is generally known that anionic and cationic surfactants cannot be mixed since they are precipitated on mixing<sup>2,3</sup>. However, many recent studies have shown that mixture of anionic and cationic surfactants can be present stable state and show synergetic properties<sup>4-6</sup>. The mixture of dodecyl benzene sulfonate and quaternary ammonium chloride shows stable state as mixed micelle and provides an excellent suspension, rheological and anti-washout properties after application to cement grouting system<sup>6-8</sup>.

Cement mortar and concrete are the construction material and generally a mixture of water, cement, sand and sometimes

fine gravel<sup>9</sup>. In the cement mortar suspension, water and cement mixture, various surfactants systems can be applied to keep mixing the components of them and prevent them from settling out. The application of the surfactants provides the pseudo-plastic properties to cement grout<sup>10,11</sup>. Additionally, anti-washout property is observed when suitable surfactant systems are applied to cement grout. The thixotropic cement mortar shows the good flow performance, placement at depositing. The thixotropic cement grout by application of suitable anionic and cationic surfactant mixtures also provide the adequate pumping pressure and the stability level after placement and consolidation during the dormant period and further more the final concrete hardness increase<sup>10-16</sup>.

When cement mortar is applied to marine construction at low temperature below 0 °C, the flow performance, workability, placement, antiwashout and consolidation should be considered in combination. Marine environment indicates the environment surrounded by seawater. Seawater is a complex solution of many salts. The average salt concentration is 3.5 %. The salts in seawater decrease the freezing point to below 0 °C. We have studied the application of surfactant admixture system to cement mortar that provides anti-washout property, self

†Presented at The 7th International Conference on Multi-functional Materials and Applications, held on 22-24 November 2013, Anhui University of Science & Technology, Huainan, Anhui Province, P.R. China

consolidation for good deformability and high resistance for segregation in cold sea water. This article provides the possible development of surfactant admixtures for concrete grouting agent for low temperature workability.

## EXPERIMENTAL

**Cement:** The cement used in this study was commercial 'Portland Type I' cement. The chemical compositions and physical properties of the cement are given in Table-1. It is composed of SiO<sub>2</sub> (20 %), Al<sub>2</sub>O<sub>3</sub> (5.3 %), CaO (62.7 %), Fe<sub>2</sub>O<sub>3</sub> (3.7 %), MgO (3 %) and small amounts of Na<sub>2</sub>O, K<sub>2</sub>O, *etc.* The density of it is 3.22 g/cm<sup>3</sup> and the surface area is 2,800 g/cm<sup>2</sup>.

**Preparation of cement grout:** Cement mortar refers to the Portland cement slurry without sand or gravel in this study. Cement mortar was prepared by the mixing of mixed surfactants solution and Portland cement<sup>7</sup>. Cationic surfactant used in this experiment was tetraalkyl ammonium chloride (QAC, 25 %, FW 320, Aldrich). Dialkyl benzene sulfonate-Na (DBS, 40 %, FW 208.21, Aldrich) was used as an anionic surfactant. Poly(methyl vinyl ether) solution (50 %, Aldrich) was applied as polymeric additives. Mixed surfactants by varying the mole ratios of anionic surfactant to cationic surfactant were prepared at 45 °C. Cement mortar was prepared by adding the mixed surfactant solution (1-2 wt %) to water and cement (W/C = 0.5) and mixing vigorously at room temperature by hand mixer.

**Artificial seawater:** For this study, artificial seawater was prepared by adding various salts to water as shown in Table-2<sup>17</sup>.

**Testing of cement mortar properties:** The viscosity changes of mortars were conducted by using a commercially available Brookfield rotational viscometer by changing the temperature from room temperature to below 0 °C.

By adding an antiwashout admixture to concrete, its viscosity is increased and its resistance to segregation is enhanced. Acryl chamber (15 cm × 4.5 cm × 20 cm) was used for the test of antiwashout properties of the mortars.

**Measurement of compressive strength of the concrete:** The compressive strength of the concrete is the capacity of structure to withstand loads tending to reduce size. The test is done for knowing the compressive strength of hardened concrete. For this purpose, concrete specimens are prepared by cylinder mold (100 mm × 200 mm) concrete in laboratory. Concrete compressive strength requirements can vary from 17 MPa for residential concrete to 28 MPa and higher in commercial structure. Cylinders tested for acceptance and quality

control are made and cured in accordance with procedures described for standard cured specimens in ASTM C 31 Standard Practice for Making and Curing Test Specimens in The Field. Cylindrical specimens are tested in accordance with ASTM C 39, Standard Test Method for Compressive Strength of Cylindrical Concrete Specimens. After casting, all specimens were left in molds and cured in the air or in the seawater. The tests were performed at age of 7, 15 and 28 days. For each age, the compressive strength was averaged from three specimens tested.

## RESULTS AND DISCUSSION

Cement mortar mixed both cationic and anionic surfactants exhibits shear-thinning behaviour whereby apparent viscosity decreases with the increase of shear rate. The mortar containing such a property is called thixotropic concrete where the viscosity buildup is promoted due to the association and entanglement of different charge properties at a low shear rate that can decrease the flow and increase the viscosity. Fig. 1 shows the viscosity of the mortar as the molar ratio of tetraalkyl ammonium chloride to dialkyl benzene sulfonate-Na changes. As the tetraalkyl ammonium chloride ratio increases the viscosity increases, whereas as the dialkyl benzene sulfonate-Na ratio increases the viscosity decreases. When the molar ratio of tetraalkyl ammonium chloride to dialkyl benzene sulfonate-Na was 1.2-1.0 or 1-1, the antiwashout properties of the mortar were observed at minimum amount amounts applied (Fig. 1).

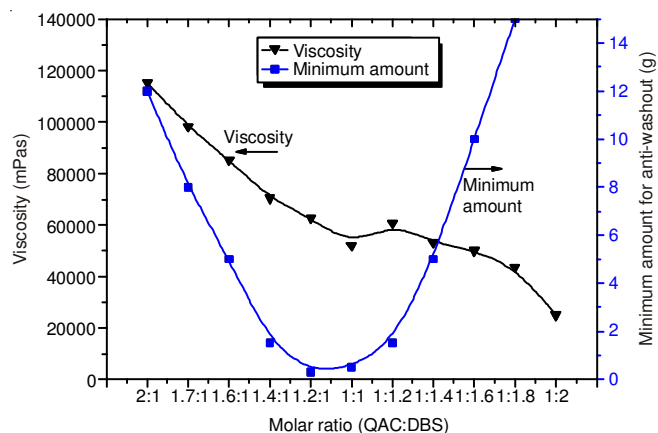


Fig. 1. Viscoelastic changes as the molar ratio of QAC/DBS changes

Table-3 shows the freezing temperature of mortar decrease by solvent addition. When 2-propanol is added by 20 % to mixed surfactant system (the composition of QAC/DBS/

TABLE-1  
CHEMICAL COMPOSITIONS AND PHYSICAL PROPERTIES OF CEMENT

Chemical composition						Physical properties		
SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	CaO	MgO	Na <sub>2</sub> O	Free limes	Density (g/cm <sup>3</sup> )	Surface area (cm <sup>2</sup> /g)
20	5.3	3.7	62.7	3	2.1	3.2	3.22	2,800

TABLE-2  
CHEMICAL COMPOSITION OF ARTIFICIAL SEAWATER

Compound	NaCl	MgCl <sub>2</sub>	Na <sub>2</sub> SO <sub>4</sub>	CaCl <sub>2</sub>	KCl
Concentration (g/L)	24.53	5.2	4.09	1.16	0.695
Compound	NaHCO <sub>3</sub>	KBr	H <sub>3</sub> BO <sub>3</sub>	SrCl <sub>2</sub>	NaF
Concentration (g/L)	0.201	0.101	0.027	0.025	0.003

TABLE-3  
FREEZING TEMPERATURE DECREASE BY SOLVENT ADDITION

Sample No.	Solvent	Wt % in mixed micelle (%)	Ratio (QAC: DBS)	Freezing test			
				0 °C	-3 °C	-6 °C	-9 °C
1	Methanol	10	1.2:1	F	F	I	I
2	Methanol	10	1:1	I	I	I	I
3	Methanol	20	1.2:1	F	F	F	F
4	Methanol	20	1:1	I	I	I	I
5	Ethanol	10	1.2:1	F	I	I	I
6	Ethanol	10	1:1	I	I	I	I
7	Ethanol	20	1.2:1	F	F	F	I
8	Ethanol	20	1:1	I	I	I	I
9	1-Propanol	10	1.2:1	I	I	I	I
10	1-Propanol	10	1:1	I	I	I	I
11	1-Propanol	20	1.2:1	F	I	I	I
12	1-Propanol	20	1:1	I	I	I	I
13	2-Propanol	10	1.2:1	I	I	I	I
14	2-Propanol	10	1:1	I	I	I	I
15	2-Propanol	20	1.2:1	F	F	F	F
16	2-Propanol	20	1:1	I	I	I	I
17	<i>n</i> -Butanol	10	1.2:1	I	I	I	I
18	<i>n</i> -Butanol	10	1:1	I	I	I	I
19	<i>n</i> -Butanol	20	1.2:1	F	F	F	F
20	<i>n</i> -Butanol	20	1:1	I	I	I	I
21	<i>n</i> -Heptanol	10	1.2:1	F	F	I	I
22	<i>n</i> -Heptanol	10	1:1	F	I	I	I
23	<i>n</i> -Heptanol	20	1.2:1	I	I	I	I
24	<i>n</i> -Heptanol	20	1:1	F	F	I	I
25	<i>n</i> -Octanol	10	1.2:1	F	F	I	I
26	<i>n</i> -Octanol	10	1:1	F	I	I	I
27	<i>n</i> -Octanol	20	1.2:1	F	F	I	I
28	<i>n</i> -Octanol	20	1:1	F	I	I	I
29	<i>n</i> -Hexane	10	1.2:1	I	I	I	I
30	<i>n</i> -Hexane	10	1:1	I	I	I	I
31	<i>n</i> -Hexane	20	1.2:1	F	F	I	I
32	<i>n</i> -Hexane	20	1:1	I	I	I	I

F = Flow as slurry; I = Frozen as an ice.

PMVE/IPA = 1.2/1/0/0.05/0.44), the freezing temperature was decreased to below -9 °C. Fig. 2 shows that the addition of mixed surfactant admixture to cement mortar increases its thixotropic, suitable antiwashout, proper workability and self-leveling properties. When mixed surfactant admixture is applied to cement mortar, the slurry was leveled without washout to water (Fig. 2a).

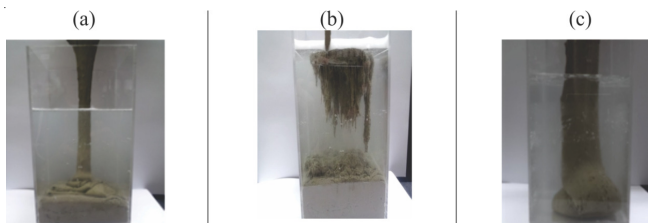


Fig. 2. Antiwashout properties at -3 °C in the seawater grouting. (a) W/C = 0.5, sample 15, (b) W/C = 0.5, no mixed surfactant admixture and (c) W/C = 0.5, after addition of commercial anti washout admixture by 2 wt %

Fig. 3 shows the viscosity changes of the mortar at different temperature. The viscosity properties at low temperature can be controlled by IPA content applied to cement mortar. Fig. 4 shows the compressive strength as the curing time changes. As the concentration of mixed surfactant admixture

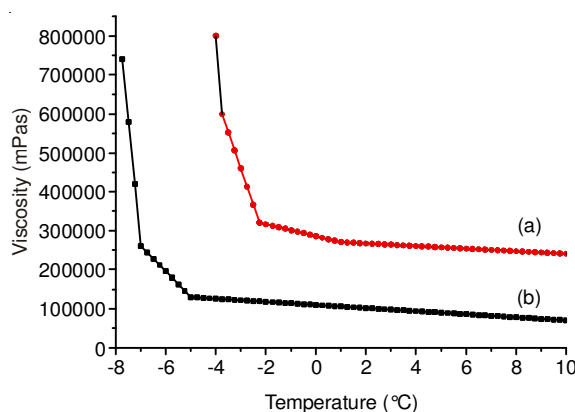


Fig. 3. Viscosity changes as the temperature of concrete mortar decrease. (a) QAC/DBS/PVME = 1.2/1/0/0.05, 1 wt % applied to W/C = 0.5 mortar (b) QAC/DBS/PVME/IPA = 1.2/1/0/0.05/0.44, 1 wt % applied to W/C = 0.5 mortar

increases, the compressive strength increases. We suggest that the concrete is packed densely and cured strongly as the mixed surfactant admixture introduction increases. The compressive strength was above 20 MPa when 1 % of the mixed surfactant admixture is applied to cement mortar and cured in the air. The strength slightly increases as curing time increases. As the mortar is cured in the seawater, it takes a month to reach the compressive strength more than 20 MPa (Fig. 5).

TABLE-4  
COMPRESSIVE STRENGTH RATIO AT CURING CONDITION (SEAWATER/AIR)

7day		15day		28day	
Wt % in mortar (%)	Seawater/air (%)	Wt % in mortar (%)	Seawater/air (%)	Wt % in mortar (%)	Seawater/air (%)
0.50	83	0.50	80	0.50	86
0.75	80	0.75	85	0.75	90
1.00	87	1.00	90	1.00	86

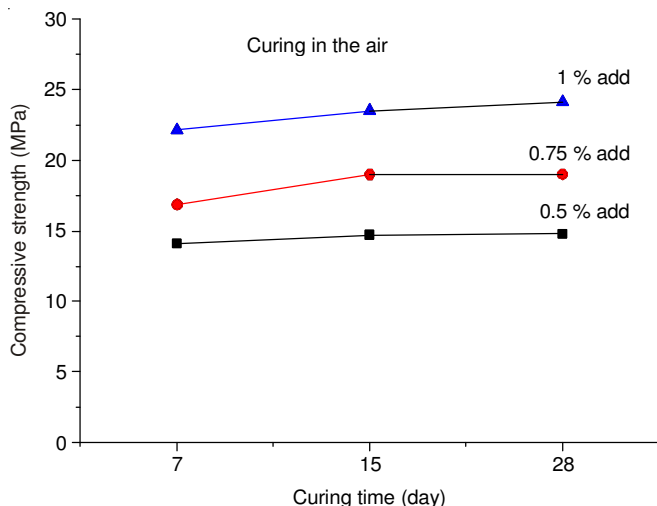


Fig. 4. Compressive strength of cement mortar after curing in the air

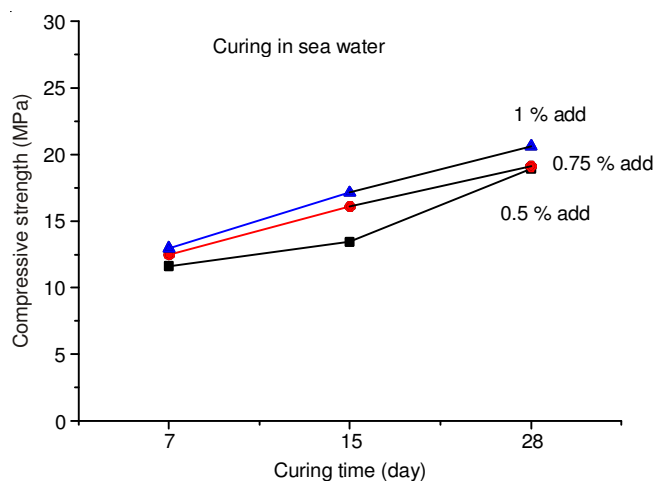


Fig. 5. Compressive strength of cement mortar after curing in the seawater

Table-4 shows the compressive strength ratio at curing in the seawater and in the air. As the mixed surfactant admixture added to concrete mortar by 0.5-1.0 wt %, 20 % decrease of compressive strength curing in the seawater was observed.

## Conclusion

Cement mortar mixed both cationic and anionic surfactants exhibits thixotropic properties. When the molar ratio of tetraalkyl ammonium chloride to dialkyl benzene sulfonate-Na was 1.2:1 or 1:1, the antiwashout properties of the mortar were observed at minimum amount amounts applied. The freezing temperature can be reduced by adding solvent such as 2-propanol to below  $-5^{\circ}\text{C}$ . The viscosity properties of the mortar at low temperature can be controlled by IPA content applied to cement mortar. The compressive strength was above 20 MPa when 1 % of the mixed surfactant admixture is applied to cement mortar and cured in the air. However, the strength was reduced by 20 % after curing in the seawater.

## ACKNOWLEDGEMENTS

This study was supported by Korean Research Council for Industrial Science and Technology (2012-0106).

## REFERENCES

1. J. Falbe, *Surfactants in Consumer Products*; Springer-Verlag Berlin Heidelberg: New York, Ch. 4 (1987).
2. G. Kume, M. Gallotti and G. Nunes, *J. Surfact Deterg.*, **11**, 1 (2008).
3. K.L. Stellner and J.F. Scamehorn, *J. Am. Oil Chem. Soc.*, **63**, 566 (1986).
4. M.J. Rosen, *Surfactant and Interfacial Phenomena*, Wiley, New York edn 2, Ch. 1-3 (1989).
5. M.J. Rosen and X.Y. Hua, *J. Am. Oil Chem. Soc.*, **59**, 582 (1982).
6. A. Upadhyaya, E.J. Acosta, J.F. Scamehorn and D.A. Sabatini, *J. Surfact. Deterg.*, **9**, 169 (2006).
7. I.K. Jang, S.R. Seo and S.K. Park, *Appl. Chem. Eng.*, **23**, 480 (2012).
8. Y. Hotaka, K. Koji and S. Daisuke, US Patent 8,105,500 B2 (2012).
9. Y.H. Kim, *Appl. Chem. Eng.*, **21**, 457 (2010).
10. W.C. Jau and C.T. Yang, *Cement Concr. Compos.*, **32**, 450 (2010).
11. K.H. Khayat and J. Assaad, *ACI Mater. J.*, **100**, 185 (2003).
12. V.H. Nguyen, S. Remond and J.L. Gallias, *Cement Concr. Res.*, **41**, 292 (2011).
13. S.H. Bae, J.I. Park and T.D. Kim, *J. Korean Soc. Urban Environ.*, **10**, 259 (2010).
14. H. El-Chabib, M. Nehdi and M. Sonebi, *ACI Mater. J.*, **100**, 165 (2003).
15. J.J. Assaad and C.A. Issa, *Constr. Build. Mater.*, **30**, 667 (2012).
16. C.F. Ferraris, *J. Res. Natl. Inst. Stand. Technol.*, **104**, 461 (1999).
17. M.M. Islam, M.S. Islam, B.C. Mondal and M.R. Islam, *J. Civ. Eng.*, **28**, 129 (2010).