

# Synthesis of FeAl/Al<sub>2</sub>O<sub>3</sub> Composites by Thermite Reaction<sup>†</sup>

YIN LIU<sup>\*</sup>, QIAN QIAN, CHUYANG XU, FANFEI MIN and MINGXU ZHANG

School of Materials Science and Engineering, Anhui University of Science and Technology, Huainan 232001, Anhui Province, P.R. China

\*Corresponding author: E-mail: yinliu@aust.edu.cn

AJC-13257

FeAl/Al<sub>2</sub>O<sub>3</sub> composites were synthesized by using *in-situ* thermite reaction of iron oxide and aluminum powder mixtures. The phase, microstructure of the composites were investigated by X-ray diffractometry, scanning electron microscopy combined with differential scanning calorimetry. The results show that a chemical rection in Fe<sub>2</sub>O<sub>3</sub>/Al system is possible and the FeAl/Al<sub>2</sub>O<sub>3</sub> composites with the interpenetrating network structure are obtained calcined at 900 °C for 60 min.

Key Words: FeAl/Al<sub>2</sub>O<sub>3</sub> composites, Microstructure, Thermite reaction.

### **INTRODUCTION**

Alumina, as an excellent construction ceramics, possesses the attractive properties of good hardness, chemical stability, refractory character and low density. However, it is brittle at low temperature for the lack of fundamental dislocation mobility and insufficient slip systems<sup>1</sup>. From the standpoint of material design, it is undoubtedly a good method to develop ceramic-matrix composite with metal or alloy dispersion because of their high strength and multi-functional properties<sup>2,3</sup>. Among the metal or alloy, the intermetallic compound FeAl possesses a high melting temperature (1250 °C), good oxidation resistance, relatively low density (5.56 g·cm<sup>-3</sup>) and high thermal conductivity. These properties make FeAl alloy a promising candidate for high temperature structural applications<sup>4,5</sup>. In addition, FeAl alloy has also been identified that its thermodynamics is compatible with alumina<sup>6</sup>.

Recently, the alumina-metal composites were synthesied by many techniques, such as reactive milling<sup>7</sup>, reactive metal infiltration<sup>8</sup>, directed metal oxidation<sup>9</sup>, reactive sintering<sup>10</sup>, thermomechanical powder consolidation processes 11, thermite reaction synthesis<sup>12-14</sup>. Among these techniques, the thermite reaction method is an attractive technique, which utilizes the exothermicity of solid-state reaction to produce advanced materials. It shows many advantages of relatively simple equipment, low energy and possibility to form intermediate phase. In the present paper, FeAl/Al<sub>2</sub>O<sub>3</sub> composites were synthesized by using *in situ* thermite reaction method. Their microstructure of FeAl/Al<sub>2</sub>O<sub>3</sub> composites were investigated.

## **EXPERIMENTAL**

Reagent grade aluminum powders (*ca.* 74  $\mu$ m) and iron oxide powders were weighed according to 4-6 molar ratio. The powders were thoroughly mixed by a planetary mill for 15 h and then the mixtures were pressed to pellets with a diameter of 32 mm under a uniaxiasl pressure of 60 MPa. The green compacts were calcined at 700, 850, 900 °C for 1 h, respectively.

The phase of samples were identified by the X-ray diffraction spectrometer using  $CuK_{\alpha}$  radiation (XRD-6000, Shimadzu). Its microstructure was observed through the scanning electron microscope (SEM, JSM-5900). The main constituent elements were determined by energy dispersive X-ray spectroscopy equipped in SEM. Thermal analyses were carried out by differential scanning calorimetry (SDT 2960, TA Co.).

### **RESULTS AND DISCUSSION**

**Phase of FeAl/Al<sub>2</sub>O<sub>3</sub> composites:** Fig. 1 shows XRD patterns of the samples obtained at different temperatures. It is found that the major phase of sample calcined at 700 °C are Fe<sub>2</sub>O<sub>3</sub> and Al. Diffraction peaks referred to Al<sub>2</sub>O<sub>3</sub>, Fe and/or FeAl are observed as it was calcined at 850 °C for 1 h, which means that the chemical reaction in Fe<sub>2</sub>O<sub>3</sub>/Al system was initiated. It can be seen that all diffraction peaks are identified to be Al<sub>2</sub>O<sub>3</sub> and FeAl as it was calcined at 900 °C for 1 h. No other impurity peak is detected in the samples.

Microstructure of FeAl/Al<sub>2</sub>O<sub>3</sub> composites: Fig. 2 shows SEM images of samples calcined at different temperatures.

\*Presented to the 6th China-Korea International Conference on Multi-functional Materials and Application, 22-24 November 2012, Daejeon, Korea



Fig. 2. SEM images of samples calcined at different temperatures. a) 700 °C, b) 850 °C, c) 900 °C

Firstly, aluminium begins to melt and spread on the surface of  $Fe_2O_3$  particles at 700 °C [Fig. 2 (a)]. According to compositions of the samples (Table-1), it is verified that the gray region A is  $Al_2O_3$  particles and white region B is FeAl particles in Fig. 2(b). The microstructure of  $Fe_2O_3/Al$  system becomes dense for the chemical reaction of  $Fe_2O_3/Al$  system was initiated at 850 °C. Fig. 2(c) shows a typical image of a sample calcined at 900 °C for 1 h and one can see that FeAl/Al<sub>2</sub>O<sub>3</sub> composites with interpenetrating networks structure can be obtained.



Fig. 1. XRD patterens of samples calcined at different temperatures for 1 h

| TABLE-1                                      |       |       |               |               |  |  |  |  |  |
|--|-------|-------|---------------|---------------|--|--|--|--|--|
| COMPOSITIONS OF THE REGIONS IN Fig. 2 (Wt %) |       |       |               |               |  |  |  |  |  |
| Region                                       | Al    | Fe    | Other element | Total content |  |  |  |  |  |
| A  | 90.31 | 7.50  | 2.19          | 100           |  |  |  |  |  |
| В  | 49.66 | 47.66 | 2.37          | 100           |  |  |  |  |  |
| С  | 44.00 | 53.79 | 2.21          | 100           |  |  |  |  |  |

**Differential scanning calorimetry analyses:** Fig.3 shows the differential scanning calorimetry curve of the green compact at heating rate of 10 °C/min. There are one endothermic peak ( $P_{Endo}$ ) and one exothermic peak ( $P_{Exo}$ ) in the curve. The observed endothermic peak locating at 660 °C can be reasonably ascribed to the melting of aluminium, the exothermic peak can be ascribed to the thermite reaction of Fe<sub>2</sub>O<sub>3</sub>/Al system.

The standard free energy of formation<sup>15</sup> can be given by:

$$\Delta G^{0}_{f} = -RT \ln k_{T}$$
(1)



Fig. 3. Differential scanning calorimetry curves of Fe<sub>2</sub>O<sub>3</sub>/Al powder mixture at heating rates of 10 °C/min

where T is temperature,  $k_T$  is equilibrium constant, for  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>,  $\Delta G^0_f = -1120500 + 214.2 \text{ T}$ , while for Fe<sub>2</sub>O<sub>3</sub>, = -540600 + 170.3 T. The standard free energy of the formation ( $\Delta G^0_f$ ) of  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> and Fe<sub>2</sub>O<sub>3</sub> versus temperature is calculated and shown in Fig. 4.

The following equation is employed to predict strictly if the chemical reaction occurs:

$$\Delta G_{f} = \Delta G_{f}^{0} + RT \ln \frac{a_{Fe}}{a_{Al}^{2}}$$
(2)

and  $a_{Fe}$  and  $a_{A1}$  are the activities of iron and aluminum in the system. Generally, it is reasonable to predict from  $\Delta G^{0}_{f}$  if the



Fig. 4. Standard free energy of the formation of  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> and Fe<sub>2</sub>O<sub>3</sub> conclusions

reaction occurs, when  $\Delta G_{\rm f}^0$  is negative and its absolute value is large enough. Fig. 4 shows the possibility of the chemical reaction in Fe<sub>2</sub>O<sub>3</sub>/Al system.

 $Fe_2O_3/Al$  system is well known by the exothermic reaction, as it is submitted to thermal treatments. The thermite reaction equation is:

$$Fe_2O_3 + 2Al \rightarrow 2Fe + Al_2O_3$$
 (3)

and the enthalpy is:

$$\Delta H_{\rm T} = \Delta H_{\rm O} + \left[ \Delta C_{\rm P} dT \right] \tag{4}$$

where  $\Delta H_0$  is the enthalpy at standard state. The  $\Delta H_0$  is - 847.63 kJ·mol<sup>-1</sup> Al<sub>2</sub>O<sub>3</sub> for eqn. 3.  $\Delta C_p$  is the difference of the heat capacity between the products and the reactants and for reaction eqn. 3.  $\Delta C_p = a + b \cdot 10^{-3}T + c \cdot 10^{5}T^{-2}$ . Table-2 gives the values of  $\Delta H_T$  for difference temperatures. It is also verified that there are strong exothermic effect in Fe<sub>2</sub>O<sub>3</sub>/Al system. Actually, the FeAl/Al<sub>2</sub>O<sub>3</sub> composites are obtained, which is attributed to the thermite reaction of Fe<sub>2</sub>O<sub>3</sub>/Al system.

| TABLE-2   EXOTHERMIC VALUES OF REACTION Eq. (3) |         |         |         |         |         |  |  |  |  |
|---|---------|---------|---------|---------|---------|--|--|--|--|
| AT DIFFERENT TEMPERATURES                       |         |         |         |         |         |  |  |  |  |
| Temperature T (K)                               | 933     | 1000    | 1100    | 1200    | 1300    |  |  |  |  |
| $\Delta H (kJ \cdot mol^{-1}Al_2O_3)$           | -911.91 | -900.56 | -916.96 | -935.32 | -955.13 |  |  |  |  |
|   |         |         |         |         |         |  |  |  |  |

#### Conclusion

Aluminum and iron oxide powders were used to prepare FeAl/Al<sub>2</sub>O<sub>3</sub> composites by *in situ* thermite reaction. The chemical reaction is feasible thermodynamically in Fe<sub>2</sub>O<sub>3</sub>/Al system. Thermite reaction in Fe<sub>2</sub>O<sub>3</sub>/Al system is ignited as the temperature is above 850 °C. FeAl/Al<sub>2</sub>O<sub>3</sub> composites with interpenetrating network structure are obtained at temperature of 900 °C for 1 h.

#### ACKNOWLEDGEMENTS

This work was supported by National Nature Science Foundation of China (51174006), Anhui Provincial Natural Science Foundation, China (1208085ME84) and The Projectsponsored by SRF for ROCS, SEM.

#### REFERENCES

- W.D. Kingery, H.K. Bowen and D.R. Uhlmaon, Introduction to Ceramics, John Wiley & Sons (1976).
- D. Manfredi, M. Pavese, S. Biamino, P. Fino and C. Badini, *Comp. Sci. Tech.*, 69, 1777 (2009).
- 3. Y. Ji and J.A. Yeomans, J. Eur. Ceram. Soc., 22, 1927 (2002).
- 4. I. Baker and P.R. Munroe, Int. Mater. Rev., 5, 181 (1997).
- 5. I. Baker, Mater. Sci. Eng. A, 192-193, 1 (1995).
- 6. H. Choo, P. Nash and M. Dollar, *Mater. Sci. Eng. A*, **239-240**, 464 (1997).
- 7. T. Venugopal, K.P. Rao and B.S. Murty, *Mater. Sci. Eng. A*, **393**, 382 (2005).
- F. Wagner, D.E. Garcia, A. Krupp and N. Claussen, J. Europ. Ceram. Soc., 19, 2449 (1999).
- 9. X. Gu and R.J. Hand, J. Eur. Ceram. Soc., 9, 823 (1995).
- 10. Z.C. Chen, T. Takeda and K. Ikeda, Comp. Sci. Tech., 68, 2245 (2008).
- A. Mukhtar, D.L. Zhang, C. Kong and P. Munroe, J. Mater. Sci., 45, 4594 (2010).
- 12. S.M. Umbrajkar, C.M. Chen, M. Schoenitz and E.L. Dreizin, *Thermochim. Acta*, **477**, 1 (2008).
- 13. H.X. Zhu and R. Abbaschian, Mater. Sci. Eng. A, 282, 1 (2000).
- Y. Liu, X.N. Fan, M.X. Zhang and X.Y. Qin, J. Wuhan Univ. Tech.-Mater. Sci. Ed., 20, 90 (2005).
- Y.J. Liang, Physical Chemistry, Metallurgy Industry Press, Beijing, China (1986) (in Chinese).